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Particle Characterisation in Geological Applications

Stephan Sanetra

1 State of the art

Measurements of the particle size distribution and characterisation of shape is one of the necessary tasks in order to describe sediments and soil samples in detail (SCHEFFER & SCHACHTSCHABEL 2002). After pretreatment of unconsolidated rocks like drying, gentle comminution of lumps and removal of biological material as well as removal of soluble salts (ISO 11464 2006), the classic method for measurements of the particle size distribution is regulated by several standards (DIN 19683 Blatt 2 1973, DIN 18123 1971, DIN 66115 1983, DIN ISO 1299 2000). Most of them are related to the German nomenclature for grain size fractions of soils and sediments (Scheffer & Schachtschabel 2002). Classic methods for measurements of broadly distributed samples always require a separation into at least one fine and one coarse fraction.

The common procedure can be described as follows:

Weighting of the pretreated sample-sieve analysis (manually or sieve shaker) at 2 mm-recording the mass of the coarse amount-wet-sieving of the fraction < 2 mm at 63 microns-drying and recording the mass of the fraction between 63 microns and 2 mm-measurements of the fraction < 63 microns using a sedimentation method (e.g. Andreasen Pipette, Köhn Pipette or Areometer application)-synthesis of sieve- and sedimentation results.

One essential disadvantage of sedimentation methods is the long measuring time, sometimes lasting longer than one day. In addition it is questionable, how the density of a sample containing different minerals can be determined precisely. Another disadvantage is the missing information on the shape of the particles: Especially in humid climate zones the process of siallitic alteration is responsible for an enrichment of clay minerals in the soil and the finer fractions often reveal essential amounts of kaolinite, montmorillonite, illite, etc.(Röllig 1971). These minerals belong to the so-called phyllosilicates (or layer silicates), which are composed of [SiO₄] tetrahedrons combined with Al-octahedrons. A determination of shape varies frequently from particle to particle. The reason for the "random" shape is, that the fit between the network of tetrahedral and octrahedral sheets is based on weak Van der Waals forces, thus the fits are not exact, the different distortions of these sheets have an influence on the dimensions of the particles, and the sheet structure causes a flaky habit of the minerals (HATHAway 1979). Unfortunately, for the calculation of the particle size distribution with help of sedimentation technique, which uses settling velocity of the particles, the precise knowledge of the shape is needed, especially with regard to the flaky habit of the phyllosilicates, which can orientate themselves in a laminar flow in that way that their settling velocity is much slower than it should be for their volume. Hence, this effect results in a too fine calculation of the particle size distribution with respect to the reality. Laser diffraction calculates volume information based on the equivalent spherical diameter of the particles passing a laser beam in a laminar flow, so that all possible orientations are measured (DIN 13220-1 1999). Published results of particle size analyses of kaolinite, illite as well as montmorillonite revealed - as expected - much finer distributions for the results based on sedimentation technique than for results based on laser diffraction, the determination of a correction factor was not feasible and for the measurement of the particle size distribution a laser diffraction system was recommended (Berthold, LÜHMANN, KLEIN & NICKEI 2000). Missing correlation factors are also known from a comparison between sieve-pipette measurements and analyses performed with a laser diffraction system (BEUSELINCK, GOVERS, POESEN, DEGRAER & FROYEN 1998).

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2 Introduction of a new measuring method

Thus, in order to overcome the problems appearing with the classic methods, time is ripe to analyse soil samples using modern measuring techniques.

As a proposal of a modern technique, a step by step – procedure with a presentation of an accompanying sample (field Name: "sand", fig. 1) is



Fig. 1: Broadly distributed sample with the field name "sand"

given below:

- 1. Weighing the entire amount of the dry or dried sample:
- Dry sieving at 6.3 mm and recording the mass of the residue on the sieve (9.55 % > 6.3 mm)
- Wet sieving of the fraction < 6.3 mm at 63 microns, weighing and recording the mass of the dried residue (60.06 % > 63 microns)
- Measurement of the fine fraction performed with a laser diffraction instrument using a measuring range from e.g. 0.5 – 175 microns:
- Measurement of the fraction between 63 microns and 6.3 mm performed with an image analysis instrument using a measuring range from e.g. 20 – 6820 microns:(fig. 2,3).

As an outstanding innovation of this measuring technique the characterisation of the shape (as one essential criterion to identify the composition of the soil, the grade of transportation or its origin) during the analysis itself should be highlighted (fig.4).

- Merge of the results from the image analyser with those from the laser diffraction instruments under consideration of the recorded mass measured with the wet-sieving procedure (Fig. 5)
- 8. Visual determination of the maximum size (estimated maximum size: Approx. 3 cm)
- Link of the merged curve with the recorded mass of the fraction > 6.3 mm using a commercial evaluation software package (fig. 6-8).

MEASUREMENT SPECIFICATION

Product name	:	Sand
Sample preparation		Separation of the coarse fraction with a 6.3 mm sieve; wet sieving of the finer fraction (90.45 % < 6.3 mm) at 63 μ m (39.94 % < 63 μ m); sampling of the fine fraction with a pipette
Sensor	:	HELOS
Dispersing system	:	QUIXEL
Measuring range HELOS	:	R3: 0.5/0.9175 µm (f = 100.00 mm)
Mass requirement	:	200 ml of the sieved fine fraction
Start condition of measurement	:	button
Stop condition of measurement	;	10 s meas.time or 20 s real time
Time base	:	100.00 ms
Measuring time	:	10.00 s (10.00 s - 10.00 s)
Optical concentration	:	19.99 % (19.81 % - 20.21 %)
Suspension liquid	:	H ₂ O
Additive	:	Na ₄ P ₂ O ₇
Window spacing of the cuvette	:	2.00 mm
Dispersing time	:	180.00 s internal ultrasonication
Pause time after ultrasonication	:	360.00 s
Pump speed	:	30.00 %
Number of measured partial samples	:	2
Measurements per partial sample	e :	3
HELOS evaluation mode	:	HRLD

Statistical evaluation of analytical data

Product: Sand) a QUIAE		Evaluation:)		
density:	1.00 g/cm3		evaluation mode:	HRLD (5.5.0.0)		
shane factor:	1.00		contamination:	0.00 %		
somple number	90506/005		containinininoit.	0.00 /0		
Measuring conditio	nt ref10 starths	ton mdurlfs	Disnersing method	d: 7mm H2O U\$180	/160 numn30	
start condition:	button	nous, moun ros	liquid:	120	cond humboo	
stan condition.	10c mans time o	20 conditions	additions.	Na40207		
stop condition:	Tos meas.ume o	208 real time	additive.	Na4F207		
time base:	100.00 ms		ultrasonic:			
measuring duration:	10.00 (10.00 - 1	0.00) s	duration:	180.00 s		
opt. concentration:	19.99 (19.81 - 2	0.21)%	pause:	360.00 s		
			pump speed:	30.00 %		
			temperature:	30.00 °C		
			window spacing of	the cuvette: 2.00 mn	n	
Preparation:			Customer: First I	nstitute of Oceanog	raphy	
sample splitting:	no					
amount of sample:	200 ml		operator:	Hfa		
additional info:			database:	HELOS 2009		
Measurements:			Identifiers:			
2009-05-13 13:30:22	2.8230 0157 H		Sand c005			
2009-05-13 13:30:34	4.3060 0157 H		Sand c006			
2009-05-13 13:30:45	5.7120 0157 H		Sand c007			
2009-05-13 13:51:34	4.4790 0157 H		Sand d005			
2009-05-13 13:51:45	5.8540 0157 H		Sand d006			
2009-05-13 13:51:57	7.2760 0157 H		Sand d007			
upper	pct, under	standard	in band	mean size	distribution	
band limit	cumulative	deviation	different	for band (log)	density (log)	
$x_0 [\mu m]$	Q. [%]	abs. [%]	dO ₃ [%]	x. [µm]	q. ²	
0.90	1.79	0.0122	1.79	0.67	0.07	
1.10	2.56	0.0172	0.77	0.99	0.09	
1.30	3.28	0.0217	0.72	1.20	0.10	
1.50	3.94	0.0257	0.67	1.40	0.12	
2.20	5.99	0.0371	1.12	1.99	0.13	
2.60	6,99	0.0422	1.00	2.39	0.14	
3.10	8.11	0.0476	1.12	2.84	0.15	
3.70	9.30	0.0529	1.19	3.39	0.15	
4.30	10.35	0.0573	1.05	3.99	0.16	
5.00	11.40	0.0617	1.09	9.09	0.17	
7.50	14.59	0.0732	1.77	6.71	0.18	
9.00	16.12	0.0786	1.53	8.22	0.19	
10.50	17.52	0.0836	1.40	9.72	0.21	
12.50	19.34	0.0901	1.82	11.46	0.24	
15.00	21.66	0.0986	2.32	13.69	0.29	
18.00	29.03	0.1096	2.97	10.43	0.37	
25.00	32.19	0.1270	4.40	22.91	0.58	
30.00	37.77	0.1264	5.58	27.39	0.70	
36.00	44.42	0.1198	6.65	32.86	0.84	
43.00	52.12	0.1235	7.70	39.34	1.00	
51.00	60.88	0.1493	8.75	46.83	1.18	
61.00	71.38	0.1969	10.51	55.78	1.35	
87.00	90.94	0.2456	8.77	79.69	1.15	
103.00	96.26	0.1632	5.32	94.66	0.73	
123.00	98.96	0.0506	2.70	112.56	0.35	
147.00	100.00	0.0000	1.04	134.47	0.13	
175.00	100.00	0.0000	0.00	160.39	0,00	
$x_{10} = 4.10 \ \mu m \pm -0.03 \ \mu m$ $x_{50} = 4$		x ₅₀ = 41.07 µ	um +/- 0.11 μm	x ₉₀ = 85.51 µm	+/- 0.39 µm	
x16 = 8.88 µm +/- 0.08 µm		x ₈₄ = 75.93 µл	n +/- 0.39 μm	x ₉₉ = 123.99 µm +/- 1.01 µm		
Q2= 5.43 % +/- 0.03 %		O ₁₀ = 17.05 %	+/- 0.08 %	Q ₅₀ = 59.78 % +/- 0.14 %		

Fig. 2: Measurement specification and statistical evaluation based on 6 measurements of the fraction < 63 microns

MEASUREMENT SPECIFICATION

Product name		Sand				
Sample preparation		teparation of the coarse fraction with a 6.3 mm sieve vet sieving of the finer fraction (90.45 % < 6.3 mm) t 63 μm (60.06 % > 63 μm); ample splitting of the fraction between 63 μm and 6.3 mm with rotating riffler				
Sensor	:	QICPIC				
Dispersing system	:	GRADIS				
Measuring range QICPIC	;	2.00 63.0 mm - M8 (206820µm)				
Mass requirement	;	21.00 g				
Start condition of measurement	:	c.opt >= 0.01%				
Stop condition of measurement	:	25s c.opt <= 0.01% oder 1300s Real time				
Frame rate	:	100.00 Hz				
Number of frames	;	110264.00 -127466.00				
Number of measured particles	:	12471042.00 - 14501653.00				
Measuring time	:	1102.91 s - 1275.01 s				
Optical concentration	:	0.1847 % - 0.1887 %				
Feed rate VIBRI	:	5.00 %				
Funnel height	:	3.00 mm				
Slit width GRADIS	:	10 mm				
Number of measured partial samples	:	3				
measurements per partial sample	:	1				
QICPIC evaluation mode	:	FERET_MIN				
Class limits	:	M8				

Statistical evaluation of analytical data

QICPIC (Q0153) & GRADIS. 2.00 63.0 mm - M8 (20...6820µm)

Product: Sand			Evaluation:			
density:	1.00 g/cm3		evaluation mode:	FERET_MIN (5.5	.0.0)	
Sample number:	90506/005	90506/005		13646843.33		
· ·				M8		
Manuring condition: 100Hz, cont0.01%, mas5-1300r			Disnersing method:	CR 50x10mm fee	sd5.can3.vibri.c.	
freme rete:	100.00 Hz	01 /0/men/2-1/00/5am	docar:	VIDDI		
frame rate;	100.00 Hz	0.00112		VIDNI		
start condition:	c.opt >== 0.01%		feed rate:	5.00 %		
stop condition:	25s c.opt <= 0.0	1% oder 1300s Real time	gap width:	3.00 mm		
measuring duration	n: 1206.84 (1102.9	1 - 1275.01) s	height of drop:	50.00 cm		
opt. concentration:	0.1868 (0.1847 -	0.1887) %	additional info:			
Preparation:	ation: Customer: First Institute of Oceanography					
sample splitting:	VCS		operator:	Thi		
amount of samale	21.00 a		database	OICPIC Januar 20	09	
Monsuromente:	21100 8		Identifiare	Qierre sandar 10		
2000-05-25 10-10-	45 7060 0153 ()		Sand 6 3mm 101			
2009-05-25 10:19	361,7000 0155 Q		Sand 6.3mm 101			
2009-05-25 11:07:26.1240 01:53 Q Sand 6.3mm 102						
2009-03-25 13:04	51.8720 0155 Q	standard	Sand_0.3mm_103	man alar	distally set on	
upper	per. under	standard	in band	mean size	distribution	
band limit	cumulative	deviation	different	for band (log)	density (log)	
x ₀ [µm]	Q ₃ [75]	abs. [%]	aQ ₃ [%]	x _m [µm]	¶1*	
20.00	0.00	0.0000	0.00	19.14	0.00	
93,52	0,30	0.0162	0.30	29.00	0.01	
115 04	42 54	1 6886	22.43	104.39	2.36	
110.01	56.03	1 9674	17 40	176 79	1 47	
169.71	60.88	2.0770	5.04	153.00	0.70	
206.13	62.93	2.1121	2.05	187.03	0.24	
250.36	64.31	2,1101	1.38	227.17	0.16	
304.08	65,30	2.0966	0,99	275,91	0.12	
369.32	65.93	2.0897	0.63	335.12	0.07	
448.57	66.66	2.0686	0.73	407.82	0.09	
544.83	67,80	1,9762	1.14	494.36	0.14	
661.73	69.12	1.8733	1.33	600.44	0.16	
803,73	70,49	1,8180	1.37	729.28	0.16	
976.19	72.01	1.7969	1.52	885.77	0.18	
1185.65	74,14	1.6167	2.13	1075.83	0.25	
1440.07	77.38	1.3395	3.24	1306.68	0.38	
1749,08	81,89	1.0857	4.51	1587.07	0.53	
2124.39	86.38	1.0851	4.49	1927.62	0.53	
2580.23	90,48	1.1955	4.11	2341.24	0.49	
3133.89	9Z.95	1.6162	2.46	2843.62	0.29	
3806,35	94.25	1.0932	1.30	3453.79	0.15	
4623.11	96.32	0.9613	2.07	4134.90	0.25	
5015,12	33,10	1.0020	6.79	5095.03	0.33	
0020.00	100.00	0.0000	0.30	0100.31	0.11	
$x_{10} = 68.55 \ \mu m$	+/- 1.26 μm	$x_{50} = 129.96 \mu m$	+/- 3.73 μm	$x_{90} = 2574.35 \mu$	um +/- 211.86 m	
x = 84.13 um +	/- 2.02 um	x., = 1025.20 µm	+/, 91 98 um	x = 5662.70 ut	n ±6.619.06 um	

Fig. 3: Statistical evaluation based on 3 measurements of the fraction between 63 microns and 6.3 mm

EQPC 1787.854 µm FERET_MAX 2193.441 µm FERET_MAX 1293.444 µm FERET_MEAN 1956.384 µm Sphericity 0.646 Acquerity 0.646 Acquerity 0.956 Imge.sumber 848	EQPC 1692.158.pm FERET_MAX 2140.869.pm FERET_MAX 1400.619.pm FERET_MAX 1842.219.pm Spherioty 0.846 Coversity 0.946 Coversity 0	EQPC 1625.495 µm FERET_MAX 1842.665 µm FERET_MAX 1544.665 µm FERET_MAX 1743.032 µm Sphericity 0.570 Carvecity 0.525 Carvecity 0.525	EQPC 1644.395 pm FERET_MAX 2152.170 pm FERET_MIN 1359.614 pm FERET_MIN 1811.855 pm Sphericity 0.557 Appetativ 0.9357 Appetativ 0.9387 Magenmaber 1860
EQPC 1555.814 µm FERT_MAX 1988.042 µm FERT_MAX 1988.042 µm FERT_MAX 170.107 µm Spherioty 0464 Conversity 0955 Impe number 2393	EQPC 1636.311 µm FEBET_MAX 2813.005 µm FEBET_MAX 2813.005 µm FEBET_MAX 2165.91 µm Sphoridty 0.754 Convexity 0.754 Imgennaber 2913	EQPC 1524.139 µm FERIT_MAX 1709.399 µm FERIT_MAX 1509.391 µm FERIT_MAX 154.003 µm Spherikity 0.571 Convexity 0.540 Image number 3821	EQPC 1545.603 pm FERRT_MAX 1870.113 pm FERRT_MN 14464460 pm FERRT_MN 1053505 pm Sphericity 0367 Conversity 0.9355 Imagennaber 4560
EQPC 1707.333 µm FERET_MAX 1965.992 µm FERET_MIX 1965.992 µm FERET_MIX 1788.1398 Splenisty 0.398 Aupent min 0.059 Image samber 4.917	EQPC 2134.981 µm FERET_MAX 2668.115 µm FERET_MAX 1864.799µm FERET_MEX 326.037 µm Spheridty 0.334 Ayeet min 0.21 Chapter Min 0.21 Chapter Min 0.21	EQPC 1892.497 µm FERET_MAX 2310.541 µm FERET_MAX 2310.541 µm FERET_MAX 2010.644 µm Spherioly 0.526 Core to a second secon	EQPC 1785.996 pm FERET_MAX 2269.372 pm FERET_MAX 1549.234 pm FERET_MAX 1890.770 pm Sphericity 0.895 Aspect mine 0.252 Charge manber 9168
EQPC 1537.153 µm FERT_MAX 1678.723 µm FERT_MAX 1678.723 µm FERT_MAX 1590.716 µm Spleristy 0.922 Aupent atio 0.366 Convoirs 0.9671 Imge sunder 9671	EQPC 1596.964µm FEBET_MAX 2281.428µm FEBET_MAX 1281.850µm FEBET_MAX 1814.881µm Spharidy 0.5421 Aspect raio 0.542 Conventior 0.1485	EQPC 1528.155 µm FERIT_MAX 1987.786 µm FERIT_MAX 1987.786 µm FERIT_MAX 1699.63 µm Spharkity 0.575 Augest ratio 0.654 Convestor 0.6755 Convestor 13755	EQPC 1721.040 pm FEBRT_MAX 2114.575 pm FEBRT_MIA 1855.0614 pm FEBRT_MIAN 1855.060 pm Spharlity 0.882 Aspect ratio 0.6445 Convolvy 0.682 Imgenmeter 15434
EQPC 1728.000 µm FERT_MAX 2566.494 µm FERT_MIN 1278.292 µm FERT_MIN 192.2592 µm Spleristy 0.319 Aupeat ratio 0.340 Composition 0.340 Composition 0.3564	EQPC 1754.110 µm FEBET_MAX 2000.099 µm FEBET_MAX 1543.028 µm FEBET_MAX 1892.368 µm Spheridy 0.338 Aspect rule 0.231 Correction 0.231 Correction 0.231	EQPC 1832.716 µm FERT_MAX 2203.881 µm FERT_MAX 1630.874 µm FERT_MAX 1942.313 µm Sphericity 0.392 Aquect tails 0.346 C nage number 19291	EQPC 1594.563 pm FERET_MAX 2251.262 pm FERET_MAX 1363.723 m Sphericity 0.500 Convestiy 0.500 Convestiy 0.900 Convestiy 0.900

Fig.4: Image analysis, fraction between 63 μ m and 6.3 mm: Excerpt of 20 particles out of 106 particles with EQPC > 1500 μ m; total amount of measured particles: 157605

As a consequence of the measurements the sample was identified as a silty sand with a minor amount of clay and a reasonable fraction of fine gravel.

3 Conclusions

For measurements of the particle size distribution of broadly distributed sediments and soil samples a separation in fine and coarse fractions by sieve procedures is necessary. As classic measuring methods sedimentation techniques for the finest fraction and sieve procedures for the coarser fractions are mandatory. In terms of sedimentation techniques, the disadvantages like long measuring times and an overestimation of the finest fraction are reported since several years. Modern measuring techniques are able to overcome these problems, but a correlation between classic and modern methods is often not feasible.

Merged curve of the sample "Sand"

measuring system : HELOS/OUIXEL, OICPIC/GRAI	DIS, sie	eve: Merge	d curve
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	×.		0.	v	
			0/	Am um	q ₃ *
1	μΠ	0.00	/0	μ	0.02
		0,90	0.72	0,07	0,03
2		1,10	1,02	0,99	0,04
3		1,50	1,51	1,20	0,04
4		1,50	1,58	1,40	0,04
5		1,80	1,95	1,04	0,05
0		2,20	2,39	1,99	0,05
/		2,00	2,79	2,39	0,06
8		3,10	3,24	2,84	0,06
9		3,70	3,72	3,39	0,06
10		4,30	4,14	3,99	0,06
11		5,00		4,04	0,07
12		6,00	5,12	5,48	0,07
13		/,50	5,83	6,/1	0,07
14		9,00	6,44	8,22	0,08
15		10,50	7,00	9,72	0,08
16		12,50	7,73	11,46	0,10
17		15,00	8,65	13,69	0,11
18		18,00	9,84	16,43	0,15
19		21,00	11,11	19,44	0,19
20		25,00	12,90	22,91	0,24
21		30,00	15,18	27,39	0,29
22		36,00	17,89	32,86	0,34
23		43,52	21,27	39,58	0,41
24		94,72	49,43	64,21	0,83
25		115,04	64,65	104,39	1,80
26		139,73	72,81	126,79	0,97
27		169,71	76,51	153,99	0,44
28		206,13	77,74	187,03	0,15
29		250,36	78,57	227,17	0,10
30		304,08	79,16	275,91	0,07
31		369,32	79,54	335,12	0,04
32		448,57	79,98	407,02	0,05
33		544,83	80,66	494,36	0,08
34		661,73	81,46	600,44	0,09
35		803,73	82,28	729,28	0,10
36	_	976,19	83,19	885,77	0,11
37		1185,65	84,47	1075,83	0,15
38	_	1440,07	86,42	1306,68	0,23
39		1749,08	89,13	1587,07	0,32
40		2124,39	91,82	1927,62	0,32
41		2580,23	94,29	2341,24	0,29
42		3133,89	95,76	2843,62	0,18
43		3806,35	96,55	3453,79	0,09
44		4623,11	97,79	4194,90	0,15
45		5615,12	99,46	5095,03	0,20
46		6300,00	100,00	5947,71	0,06
47		30000,00	100,00	13747,73	0,00
r				T	
x ₁₀ =	20,81µm	x ₅₀ =	102.37µm	x ₉₀ =	5502.29 μm
$Q_2 =$	1.97%	$Q_{63} =$	28,99%	Q ₂₀₀₀ =	82,43%

Fig. 5: Merged curve

Merged and linked result of the Sample "Sand"

	Xo	02	X		
	μm	%	μm	q ₃ *	
1	0,90	0,65	0,67	0,03	
2	1,10	0,93	0,99	0,03	
3	1,30	1,19	1,20	0,04	
4	1,50	1,43	1,40	0,04	
5	1,80	1,76	1,64	0,04	
6	2,20	2,17	1,99	0,05	
7	2,60	2,53	2,39	0,05	
8	3,10	2,94	2,84	0,05	
9	3,70	3,37	3,39	0,06	
10	4,30	3,75	3,99	0,06	
11	5,00	4,14	4,64	0,06	
12	6,00	4,64	5,48	0,06	
13	7,50	5,28	6,71	0,07	
14	9,00	5,84	8,22	0,07	
15	10,50	6,34	9,72	0,08	
16	12,50	7,00	11,46	0,09	
17	15,00	7,84	13,69	0,11	
18	18,00	8,92	16,43	0,14	
19	21,00	10,07	19,44	0,17	
20	25,00	11,70	22,91	0,21	
21	30,00	13,76	27,39	0,26	
22	36,00	16,22	32,86	0,31	
23	43,52	19,28	39,58	0,37	
24	94,72	44,81	64,21	0,76	
25	115,04	58,60	104,39	1,63	
26	139,73	66,01	126,79	0,88	
27	169,71	69,36	153,99	0,40	
28	206,13	70,47	187,03	0,13	
29	250,36	71,23	227,17	0,09	
30	304,08	71,77	275,91	0,06	
31	369,32	72,11	335,12	0,04	
32	448,57	72,50	407,02	0,05	
33	544,85	73,13	494,30	0,07	
34	001,/3 802.72	/3,85	600,44	0,09	
33	803,73	74,39	129,28	0,09	
27	970,19	75,42	003,//	0,10	
29	1165,05	70,38	1075,85	0,14	
30	1740.08	70,33	1500,08	0,21	
40	2124.30	83.24	1027.62	0,29	
40	2124,39	85.48	2341.24	0,29	
42	3133.80	86.82	2371,24	0.16	
43	3806 35	87 53	3453 70	0,10	
44	4623 11	88.66	4194.90	0.13	
45	5615 12	90.17	5095.03	0.18	
46	6300.00	90.45	5947.71	0.06	
47	30000.00	100.00	13747.73	0.14	
• /	20000,00	100,00			

x ₁₀ =	20,81µm	x ₅₀ =	102.37µm	x90 =	5502.29 μm
Q2=	1.97%	Q ₆₃ =	28,99%	Q ₂₀₀₀ =	82,43%
Clay		Silt		Sand	
(fraction < 2)	1.97%	(fraction 2-	27,02%	(fraction 63-	53,48%
microns)		63 microns)		2000 microns	

Fig. 6: Merged and linked curve



Fig. 7: Cumulative distribution



Fig.8: Density distribution curve q_{3la}

The proposed step by step procedure in combination with the presentation of results will introduce the measurement of the particle size distribution and the characterisation of the shape with modern measuring techniques. The duration of the procedure is much shorter than the classic one and the result is not any longer based on a sedimentation method with all the oddities caused by incorrect assumptions of shape and density of the particles.

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